

Steam reforming of bio-ethanol over Ni on Ce-ZrO₂ support: Influence of redox properties on the catalyst reactivity

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Abstract

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The steam reforming of ethanol over Ni on Ce-ZrO₂ support, (Ni/ Ce-ZrO₂) were studied. The catalyst provides significantly higher reforming reactivity and excellent resistance toward carbon deposition compared to Ni/Al₂O₃ under the same conditions. At the temperature above 800°C, the main products from the reforming processes over Ni/Ce-ZrO₂ were H₂, CO, and CO₂ with small amount of CH₄ depending on the inlet ethanol/steam and oxygen/ethanol ratios, whereas high hydrocarbon compounds i.e., C₂H₄ and C₂H₆ were also observed from the reforming of ethanol over Ni/Al₂O₃ in the range of conditions studied (700-1000°C).

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These excellent ethanol reforming performances of Ni/Ce-ZrO₂ in terms of stability, reactivity and product selectivities are due to the high redox property of Ce-ZrO₂. During the ethanol reforming process, in addition to the reactions on Ni surface, the gas-solid reactions between the gaseous components presented in the system (C₂H₅OH, C₂H₆, C₂H₄, CH₄, CO₂, CO, H₂O, and H₂) and the lattice oxygen (O_x) on Ce-ZrO₂ surface also take place. Among these redox reactions, the reactions of adsorbed surface hydrocarbons with the lattice oxygen (O_x) (C_nH_m + O_x → nCO + m/2(H₂) + O_{x-n}) can eliminate the formation of high hydrocarbons (C₂H₆ and C₂H₄), which easily decompose and form carbon species on Ni surface (C_nH_m → nC + m/2H₂).

Key words : ethanol, steam reforming, autothermal reforming, solid oxide fuel cell

บทคัดย่อ

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กระบวนการรีฟอร์มมิ่งของไบโอเอทานอลด้วยน้ำบนตัวเร่งปฏิกิริยาชนิด Ni/Ce-ZrO₂ :
ผลของคุณสมบัติรีดอกซ์ต่ออัตราการเกิดปฏิกิริยา

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การศึกษากระบวนการรีฟอร์มมิ่งเอทานอลด้วยน้ำ โดยใช้ตัวเร่งปฏิกิริยาชนิด Ni/Ce-ZrO₂ (Ni บน Ce-ZrO₂) พบว่าตัวเร่งปฏิกิริยาชนิดนี้ให้ประสิทธิภาพการรีฟอร์มมิ่งที่ดี และมีความต้านทานต่อการเกิดคาร์บอน (carbon formation) สูงเปรียบเทียบกับตัวเร่งปฏิกิริยาชนิด Ni/Al₂O₃ ที่สภาวะเดียวกัน และ ณ ที่อุณหภูมิสูงกว่า 800°C พบว่าผลิตภัณฑ์หลักจากกระบวนการรีฟอร์มมิ่งด้วย Ni/Ce-ZrO₂ ได้แก่ H₂, CO, และ CO₂ โดยพบ CH₄ เพียงเล็กน้อย ขึ้นอยู่กับสัดส่วนของการป้อน เอทานอล/น้ำ และสัดส่วนของการป้อน ออกซิเจน/เอทานอล อีกทั้งยังพบว่ามีสารประกอบไฮโดรคาร์บอนอื่น ๆ เช่น C₂H₄ และ C₂H₆ จากการศึกษาการทดลองทำการรีฟอร์มมิ่งเอทานอลด้วย Ni/Al₂O₃ ในช่วงอุณหภูมิที่ศึกษา (700-1000°C)

ประสิทธิภาพของตัวเร่งปฏิกิริยา Ni/ Ce-ZrO₂ ต่อการรีฟอร์มมิ่งของเอทานอลในเชิงของ stability, reactivity, and product selectivities นั้นต่างก็ขึ้นอยู่กับคุณสมบัติการ redox ที่สูงของ Ce-ZrO₂ จากกระบวนการรีฟอร์มมิ่งเอทานอลพบว่า ปฏิกิริยาบนพื้นผิวของ Ni ระหว่างก๊าซต่าง ๆ ที่ปรากฏในระบบ (C₂H₅OH, C₂H₆, C₂H₄, CH₄, CO₂, CO, H₂O และ H₂) กับ lattice oxygen (O_x) บนพื้นผิวของ Ce-ZrO₂ ได้เกิดขึ้น (gas-solid reactions) จากปฏิกิริยารีดอกซ์ เหล่านี้ ทำให้เกิดการดูดซับที่ผิวของ hydrocarbons โดย lattice oxygen (O) (C_nH_m + O_x → nCO + m/2(H₂) + O_{x-n}) และสามารถกำจัดคาร์บอนของ high hydrocarbons (C₂H₆ และ C₂H₄) ซึ่งสามารถสลายตัวได้ง่ายและก่อให้เกิด carbon species บนพื้นผิวของ Ni (C_nH_m → nC + m/2H₂)

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Solid Oxide Fuel Cell (SOFC) is a promising energy conversion unit that produces electrical energy and heat with greater energy efficiency and lower pollutant emission than combustion processes. Hydrogen is a major fuel for SOFC. Nevertheless, the use of other hydrocarbon fuels such as methane, methanol, ethanol, gasoline and other oil derivatives is also possible when operated

as an internal or in-stack reforming. As SOFC is operated at such a high temperature, these hydrocarbons can be internally reformed producing a H₂/CO rich gas, which is eventually used to generate the electrical energy and heat.

Regarding the global environmental problems and current fossil fuel crisis, the development of Internal Reforming Solid Oxide Fuel Cell (IR-

SOFC) fed by biomass or renewable based fuels attracts more attention to be an alternative method for power generation in the near future. Among renewable sources, ethanol is a promising candidate, since it is readily produced by fermentation of biomasses and has reasonably high hydrogen content, in addition, ethanol is also safe to handle, transport and store (Cavallaro *et al.*, 1996; Athanasio *et al.*, 2004). The major difficulty to reform ethanol is the deactivation of the reforming catalyst due to the possible carbon deposition during ethanol decomposition, particularly at high temperature.

Previously, steam reforming of ethanol has been studied by several researchers (Garcia *et al.*, 2000; Srinivas *et al.*, 2003). Most of them have investigated the reforming of ethanol over noble metal catalysts (e.g. Rh, Ru, Pt, Pd) on several oxide supports (e.g. Al₂O₃, MgO, SiO₂, TiO₂) (Cavallaro *et al.*, 1996; Freni *et al.*, 2003). Verykios and coworkers (Fatsikostas *et al.*, 2002; Liguras *et al.*, 2003) reported that Rh-based catalyst provides significantly higher activity and stability toward the steam reforming of ethanol compared to Ru, Pt, Pd, and also Ni. Similarly, Freni *et al.* (Cavallaro *et al.*, 1996; Freni, 2001; Freni *et al.*, 2002) reported that Rh/Al₂O₃ provides the highest reforming reactivity among noble metal catalysts (e.g. Rh, Ru, Pt, Pd) on several oxide supports (e.g. Al₂O₃, MgO, SiO₂, TiO₂). Sobyenin and coworkers (Galvita *et al.*, 2002) studied the decomposition of ethanol in the presence of steam over Pd supported on a porous carbonaceous material, and reported that the catalyst exhibits a high activity and long-term stability. Burch and coworkers (Breen *et al.*, 2002) found that the order of ethanol steam reforming reactivity of the metals was Rh > Pd > Ni = Pt, and also reported the important role of the catalyst support. Verykios and coworkers (Fatsikostas *et al.*, 2002; Liguras *et al.*, 2003) also investigated the steam reforming of ethanol over Ni based catalyst on several oxide supports (e.g. La₂O₃, Al₂O₃, YSZ, and MgO). They revealed that Ni/La₂O₃ and Ni/La₂O₃/Al₂O₃ exhibit high activity and stability for hydrogen production.

According to the previous publications, under steam reforming conditions, an extensive formation of encapsulated carbon was always observed even if the noble metal catalysts were applied. This carbon formation was mainly due to the decomposition of ethanol forming high hydrocarbons (e.g. acetaldehyde, ethylene, and ethane), which easily formed the carbonaceous deposits. Adding oxygen as an autothermal reforming was proven to provide great benefits in terms of catalyst stability and coke suppression (Laosiripojana *et al.*, 2005); however, the yield of hydrogen production could be minimized due to the oxidation of hydrogen by oxygen added.

In this work, it was aimed to develop an alternative catalyst for steam and reforming of ethanol, which could provide high stability and activity toward this reaction at such a high temperature (700-1000°C). According to the economical point of view, Ni was selected as a catalyst rather than other precious metals such as Pt, Rh and Ru. Although the precious metals have been reported to be active for the reforming reactions and resistant to the carbon formation than Ni (Mattos *et al.*, 2003; Roh *et al.*, 2003), the current prices of these metals are very high for commercial uses, and the availability of some precious metals such as ruthenium was too low to have a major impact on the total reforming catalyst market (Rostrup-Nielsen *et al.*, 1988). Selection of a support material is the major consideration of this work. It has widely been reported that metal catalysts are not very active for the steam reforming when supported on inert oxides (Wang *et al.*, 2002). Various supports have been investigated, for example, α -Al₂O₃ (Roh *et al.*, 2002), and γ -Al₂O₃ with alkali metal oxide and rare earth metal oxide (Miao *et al.*, 1997), and CeO₂ based supports (Dong *et al.*, 2002). A promising catalyst system for the reforming reactions appeared to be a metal on CeO₂-based supports, where metals can be Ni, Pt or Pd. Therefore, Ce-ZrO₂ was chosen as catalyst support over Ni in this work.

In the present work, the stability and activity toward the steam reforming of ethanol over Ni on

Ce-ZrO₂ support (Ni/Ce-ZrO₂) was studied and compared to conventional Ni/Al₂O₃. The resistance toward carbon formation and the product selectivities over these catalysts were also studied.

Experimental

1. Catalyst preparation and characterization

Ce_{1-x}Zr_xO₂ supports with different Ce/Zr molar ratios were prepared by co-precipitation of cerium nitrate (Ce(NO₃)₃·H₂O), and zirconium oxychloride (ZrOCl₂·H₂O) (from Aldrich). The starting solution was prepared by mixing 0.1 M of metal salt solution with 0.4 M of urea at a 2 to 1 volumetric ratio. The ratio between each metal salt was altered to achieve nominal Ce/Zr molar ratios: Ce_{1-x}Zr_xO₂, where x = 0.25, 0.50, and 0.75 respectively. This solution was stirred by magnetic stirring (100 rpm) for 3 h, and the precipitate was filtered and washed with deionised water and ethanol to prevent an agglomeration of the particles. It was dried overnight in an oven at 110°C, and then calcined in air at 1000°C for 6 h.

Ni/Ce-ZrO₂ was prepared by impregnating Ce-ZrO₂ with a Ni(NO₃)₂ solution (from Aldrich). The catalyst was reduced with 10% H₂/Ar for 6 h before use. For comparison, Ni/Al₂O₃ (5wt% Ni) were also prepared by impregnating α-Al₂O₃ (from Aldrich) with Ni(NO₃)₂. After reduction, the catalysts were characterized by several physico-chemical methods. The weight content of Ni in Ni/Al₂O₃ and Ni/Ce-ZrO₂ (with different Ce/Zr ratio) were determined by X-ray fluorescence (XRF) analysis. The reducibility and dispersion percentages of nickel were measured from temperature-programmed reduction (TPR) with 5% H₂ in Ar and temperature-programmed desorption (TPD) respectively. The catalyst specific surface areas were obtained from BET measurement.

2. Apparatus and Procedures

An experimental reactor system was constructed as shown in Figure 1. The feed gases including the components of interest (ethanol and steam from the evaporator, and oxygen as the additive gas) and the carrier gas (helium) were

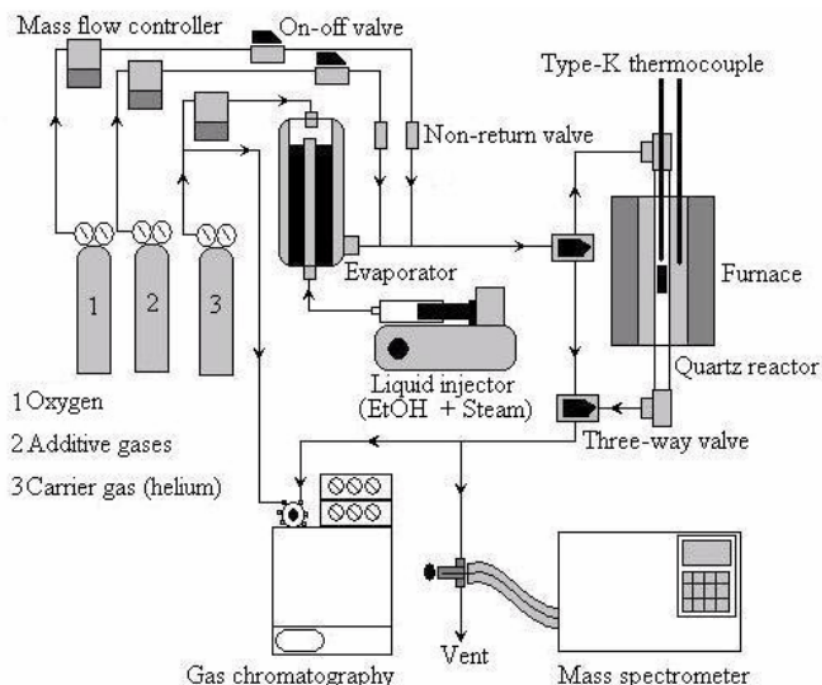


Figure 1. Schematic diagram of the experimental set-up.

introduced to the reaction section, in which an 10-mm diameter quartz reactor was mounted vertically inside a furnace. The catalyst was loaded in the quartz reactor, which was packed with a small amount of quartz wool to prevent the catalyst from moving. Regarding the results in our previous publications (Laosiripojana *et al.*, 2005; Laosiripojana, 2003), in order to avoid any limitations by intraparticle diffusion, the weight of catalyst loading was kept constant at 50 mg, while the total gas flow rate was 100 cm³ min⁻¹ under a constant residence time of 5 x 10⁻⁴ g min cm⁻³ in all experiments. A Type-K thermocouple was placed into the annular space between the reactor and the furnace. This thermocouple was mounted on the tubular reactor in close contact with the catalyst bed to minimize the temperature difference between the catalyst bed and the thermocouple. Another Type-K thermocouple was inserted in the middle of the quartz tube in order to re-check the possible temperature gradient. The record showed that the maximum temperature fluctuation during the reaction was always ±0.75°C or less from the temperature specified for the reaction.

After the reactions, the exit gas mixture was transferred via trace-heated lines to the analysis section, which consists of a Porapak Q column Shimadzu 14B gas chromatograph (GC) and a mass spectrometer (MS). The gas chromatography was applied in order to investigate the steady state condition experiments, whereas the mass spectrometer in which the sampling of the exit gas was done by a quartz capillary and differential pumping was used for the transient carbon formation experiment. In order to study the formation of carbon species on catalyst surface, Temperature Programmed Oxidation (TPO) was applied by introducing 10% oxygen in helium (100 cm³ min⁻¹) into the system, after purging with helium. The operating temperature increased from room temperature to 1000°C by the rate of 20°C/min. The calibrations of CO and CO₂ productions were performed by injecting a known amount of these calibration gases from a loop, in an injection valve in the bypass line. The response factors were obtained by dividing the number of moles for each

component over the respective areas under peaks. The amount of carbon formations on the surface of catalysts were determined by measuring the CO and CO₂ yields from the TPO results (using Microcal Origin Software) assuming a value of 0.026 nm² for the area occupied by a carbon atom in a surface monolayer of the basal plane in graphite (Ramirez *et al.*, 2002). In addition to the TPO method, the amount of carbon deposition was confirmed by the calculation of carbon balance in the system. The amount of carbon deposited on the surface of the catalyst is theoretically equal to the difference between the inlet carbon containing components (C₂H₅OH) and the outlet carbon containing components (CO, CO₂, CH₄, C₂H₆, C₂H₄, and C₂H₄O). The amount of carbon deposited per gram of catalyst is given by the following equation:

$$C_{\text{deposition}} = \frac{\text{mole}_{\text{carbon(in)}} - \text{mole}_{\text{carbon(out)}}}{m_{\text{catalyst}}} \quad (1)$$

3. Kinetic parameters formulae

The results of ethanol decomposition were shown in terms of conversion (X_{Ethanol}), and the products selectivity (hydrogen, carbon monoxide, carbon dioxide, methane, ethane, ethylene, and acetaldehyde (S_{product})), which are calculated according to Eqs. (2) - (9):

$$X_{\text{Ethanol}} = \frac{100(\% \text{Ethanol}_{\text{in}} - \% \text{Ethanol}_{\text{out}})}{\% \text{Ethanol}_{\text{in}}} \quad (2)$$

$$S_{\text{H}_2} = \frac{100(\% \text{H}_2)}{3(\% \text{Ethanol}_{\text{in}} - \% \text{Ethanol}_{\text{out}}) + (\% \text{H}_2\text{O}_{\text{in}} - \% \text{H}_2\text{O}_{\text{out}})} \quad (3)$$

$$S_{\text{CO}} = \frac{100(\% \text{CO})}{2(\% \text{Ethanol}_{\text{in}} - \% \text{Ethanol}_{\text{out}})} \quad (4)$$

$$S_{\text{CO}_2} = \frac{100(\% \text{CO}_2)}{2(\% \text{Ethanol}_{\text{in}} - \% \text{Ethanol}_{\text{out}})} \quad (5)$$

$$S_{\text{CH}_4} = \frac{100(\% \text{CH}_4)}{2(\% \text{Ethanol}_{\text{in}} - \% \text{Ethanol}_{\text{out}})} \quad (6)$$

$$S_{\text{C}_2\text{H}_6} = \frac{100(\% \text{C}_2\text{H}_6)}{2(\% \text{Ethanol}_{\text{in}} - \% \text{Ethanol}_{\text{out}})} \quad (7)$$

$$S_{C_2H_4} = \frac{100(\%C_2H_4)}{2(\%Ethanol_{in} - \%Ethanol_{out})} \quad (8)$$

$$S_{C_2H_4O} = \frac{100(\%C_2H_4O)}{2(\%Ethanol_{in} - \%Ethanol_{out})} \quad (9)$$

Results

1. Homogenous (non catalytic) reaction

Before studying performances of the catalysts, homogeneous (non-catalytic) steam reforming and autothermal reforming of ethanol were primary investigated. Regarding the steam reforming testing, inlet C₂H₅OH/H₂O in helium with the molar ratio of 1.0/3.0 was introduced to the system, while the temperature increased from 100°C to 950°C. As shown in Figure 2, it was observed that ethanol was converted to acetaldehyde, and hydrogen at the temperature above 200°C. Methane and carbon monoxide productions were initially observed at the temperature around 250-300°C. The selectivity of acetaldehyde significantly dropped at the temperature of 550°C and approached zero at the temperature of 650°C. In this range of temperature, the formations of ethane and ethylene were observed. The selectivities of carbon monoxide, carbon dioxide, methane, ethane and ethylene remained almost constant at temper-

atures higher than 650°C.

According to the testing, ethanol homogeneously converts to acetaldehyde, hydrogen, methane, and carbon monoxide via the dehydrogenation of ethanol and simultaneous fast decomposition of acetaldehyde at low temperature (300-500°C) (Eqs. 10 and 11).



When the temperature increases, the methane steam reforming and water-gas shift reactions (Eqs. 12 and 13) then take place. Ethylene is also formed by the dehydration of ethanol (Eq. 14) whereas the production of ethane is from ethylene hydrogenation (Eq. 15). This phenomenon is confirmed by the observation of lower H₂ selectivity compared to CO selectivity.

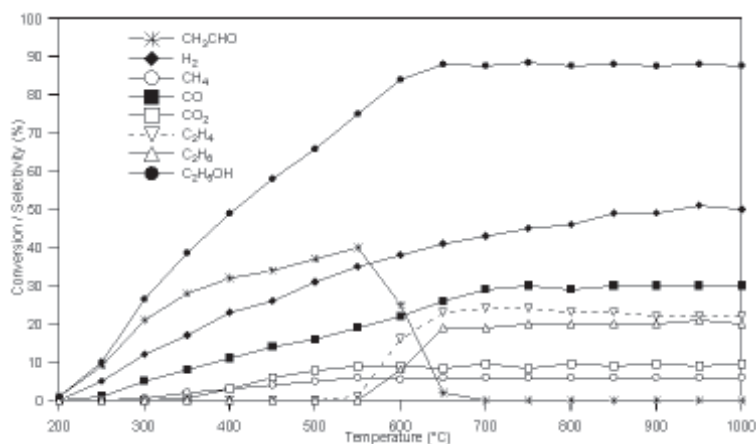
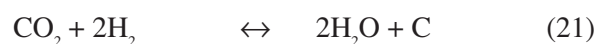
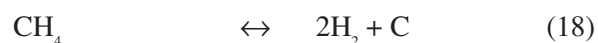
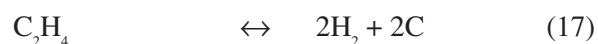
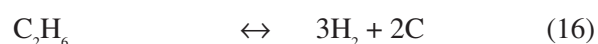


Figure 2. Homogenous (in the absence of catalyst) reactivity of ethanol steam reforming (4 kPa C₂H₅OH, and 12 kPa H₂O)

The formations of ethylene and ethane by the homogeneous decomposition of ethanol are the major difficulties for the catalytic reforming of ethanol at high temperature. It has been widely established that ethane and ethylene act as very strong promoters of carbon formation. Moreover, ethanol and methane can also be decomposed and converted to coke. Although the formations of ethylene and ethane can be reduced by adding oxygen, significant amount of these high hydrocarbons remains observed from the reaction. Eqs. 16-21 below present the most probable reactions that could lead to carbon deposition from the reforming of ethanol:



C is the carbonaceous deposits. At low temperature, Eqs. (20-21) are favorable, while Eqs. (16-19) are thermodynamically unflavored (Lwin *et al.*, 2000). The Boudard reaction (Eq. 19) and the decomposition of hydrocarbons (Eqs. 16-18) are the major pathways for carbon formation at such a high temperature as they show the largest

change in Gibbs energy. According to the range of temperature in this study, carbon formation would be formed via the decomposition of hydrocarbons and Boudard reactions. By increasing inlet steam to ethanol molar ratio, the degree of carbon formation from the steam reforming of ethanol decreases, as the equilibrium of water-gas shift reaction moves forward producing more CO₂ rather than CO and eventually avoids carbon deposition via the Boudard reaction. However, significant amount of carbon remains detected due to the decomposition of ethane, ethylene, and methane (Eqs. 8-10).

2. Ratio Selection of Ce/Zr supported on Ni/Ce-ZrO₂

After preparation, all physicochemical properties of the synthesized catalysts are characterized as presented in Table 1. For Ce-ZrO₂, XRD testing was carried out to confirm the formation of Ce-ZrO₂ as shown in Figure 3. To determine the suitable ratio of Ce to Zr for the preparation of Ni/Ce-ZrO₂, the activity testing from using different ratios was conducted at 750°C. The feed was C₂H₅OH/H₂O in helium with the molar ratios of 1.0/3.0. The ratios of Ce/Zr were 0:1, 1:3, 1:1, 3:1 and 1:0. The result in Figure 4 shows that the Ce/Zr ratio = 1:3 demonstrates the highest selectivity of hydrogen when testing at 750°C.

3. Reactivity toward ethanol steam reforming

The steam reforming of ethanol over Ni/Ce-ZrO₂ and conventional Ni/Al₂O₃ were studied at

Table 1. Physicochemical properties of the catalysts after reduction

Catalyst	Ce/Zr Ratio	Ni-load ^a (wt.%)	BET Surface Area (m ² g ⁻¹)	Ni-reducibility ^b (Ni%)	Ni-dispersion ^c (Ni%)
Ni/Ce-ZrO ₂	1/3	5.0	20	90.4	4.24
Ni/Ce-ZrO ₂	1/1	4.7	18	89.8	4.13
Ni/Ce-ZrO ₂	3/1	4.8	19	88.1	4.37
Ni/Al ₂ O ₃		4.9	40	92.1	4.87

^a Measured from X-ray fluorescence analysis.

^b Measured from temperature-programmed reduction (TPR) with 5% hydrogen.

^c Measured from temperature-programmed desorption (TPD) of hydrogen after TPR measurement.

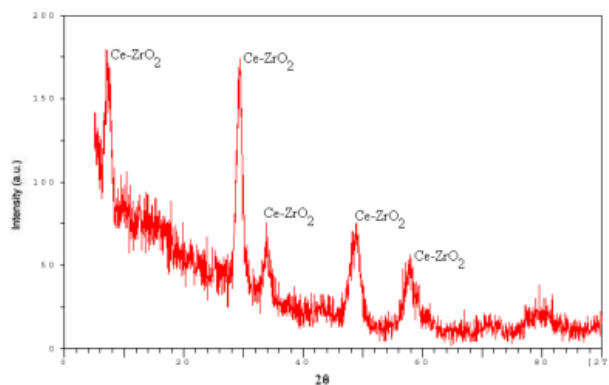


Figure 3. XRD pattern of synthesized Ce-ZrO₂

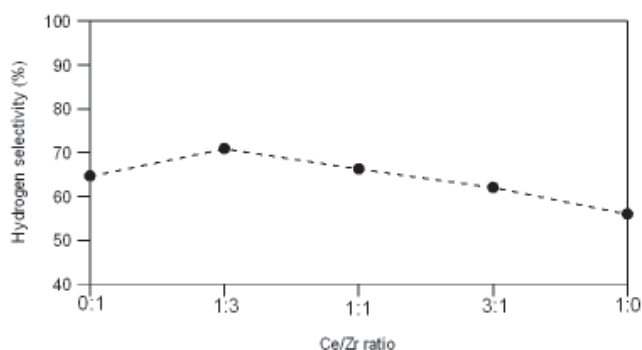


Figure 4. The percentage of hydrogen selectivity from ethanol steam reforming by varying ratio of Ce/Zr on Ni/Ce-ZrO₂ at 750°C

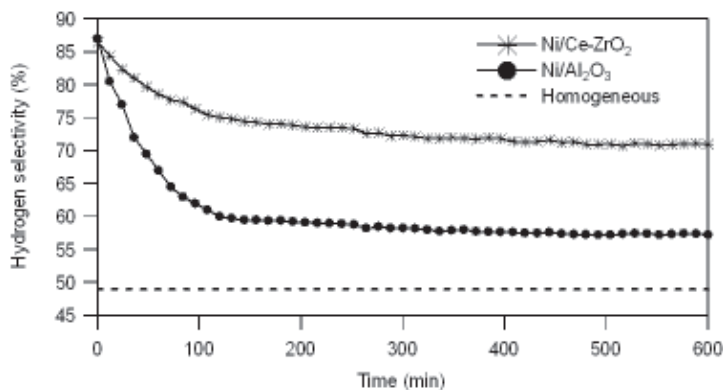


Figure 5. Steam reforming of ethanol at 750°C for Ni/Ce-ZrO₂ (Ce/Zr = 3/1) and Ni/Al₂O₃

750°C. The feed was C₂H₅OH/H₂O in helium with the molar ratios of 1.0/3.0. The variations in hydrogen selectivities (%) with time at 750°C for different catalysts are shown in Figure 5

During 10 h operation, the hydrogen selectivities of Ni/Ce-ZrO₂ were significantly higher than Ni/Al₂O₃, the hydrogen selectivity of Ni/Ce-ZrO₂ at steady state is approximately 70-75%. However, the

Table 2. Physicochemical properties of the catalysts after exposure in ethanol steam reforming at 750°C for 10 h

Catalyst	C ₂ H ₅ OH/H ₂ O ratio	Deactivation (%)	BET surface (m ² g ⁻¹)	Ni-load ^a (wt.%)	Ni-red. ^b (Ni%)	Ni-disp. ^c (Ni%)
Ni/Al ₂ O ₃ (Ce/Zr = 3/1)	1.0/3.0	17.1	17.1	4.9	90.2	4.18
	1.0/2.0	19.8	17.2	4.9	90.0	4.13
	1.0/1.0	24.6	17.1	4.7	90.2	4.17
Ni/Ce-ZrO ₂	1.0/3.0	33.2	~ 40.0	4.9	92.0	4.85
	1.0/2.0	34.6	39.5	4.9	91.7	4.87
	1.0/1.0	39.5	~ 40.0	4.8	91.8	4.87

^a Measured from X-ray fluorescence analysis^b Nickel reducibility (measured from temperature-programmed reduction (TPR) with 5% hydrogen)^c Nickel dispersion (measured from temperature-programmed desorption (TPD) after TPR)**Table 3. The dependence of inlet C₂H₅OH/H₂O ratio on the amount of carbon formation remaining on the catalyst surface after exposure in ethanol steam reforming at 750°C for 10 h**

C ₂ H ₅ OH/H ₂ O ratio	Total carbon formation (monolayers)	
	Ni/Ce-ZrO ₂	Ni/Al ₂ O ₃
1.0/3.0	1.52 ^a (1.47) ^b	4.52 ^a (4.54) ^b
1.0/2.0	1.69 (1.72)	4.76 (4.78)
1.0/1.0	1.84 (1.84)	4.81 (4.79)

^a Calculated using CO and CO₂ yields from temperature-programmed oxidation (TPO) with 10% oxygen.^b Calculated from the balance of carbon in the system.

deactivations were also observed in both catalysts. Results of the catalyst stabilities expressed as deactivation percentages and the post reaction characterizations are given in Table 2.

The post-reaction temperature-programmed oxidation (TPO) experiments were then carried out after a helium purge by introducing 10% oxygen in helium in order to determine whether the observed deactivation is due to the carbon formation. From the TPO results shown in Figure 6, small peaks of carbon dioxide and carbon monoxide were observed for Ni/Ce-ZrO₂, whereas huge amount of carbon dioxide and carbon monoxide formations were detected for Ni/Al₂O₃. The amount of carbon formations can be determined by measuring the CO and CO₂ yields from these TPO results. Using a value of 0.026 nm² for the

area occupied by a carbon atom in a surface monolayer of the basal plane in graphite (Ramirez *et al.*, 2002), the quantities of carbon deposited over Ni/Ce-ZrO₂ and Ni/Al₂O₃ were observed to be approximately 1.52 and 4.52 monolayers, respectively, for the inlet C₂H₅OH/H₂O ratio of 1.0/3.0. The degree of carbon formation was found to decrease with increasing inlet H₂O concentration as shown in Table 3.

The high resistance toward carbon deposition for Ni/Ce-ZrO₂ was reported in our previous publications (Laosiripojana *et al.*, 2005) and is mainly due to the high oxygen storage capacity (OSC) of this material. Ce-ZrO₂ contains a high concentration of highly mobile oxygen vacancies and thus acts as a local source or sink for oxygen on its surface. It has been reported that at high

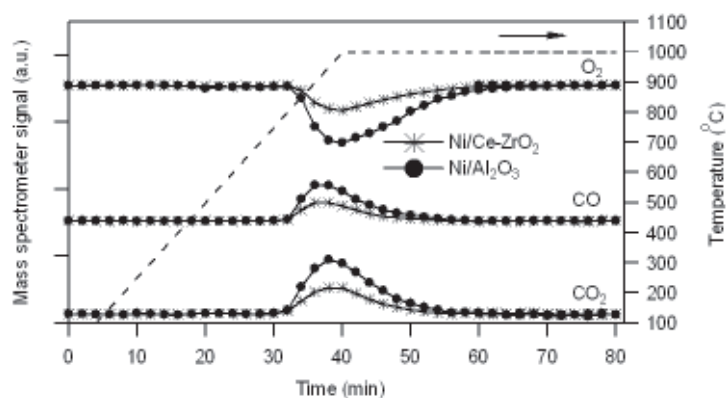
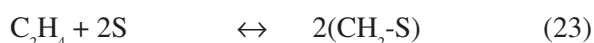
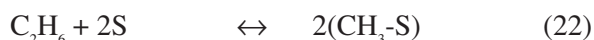


Figure 6. Temperature Programmed Oxidation (TPO) of Ni/Ce-ZrO₂ and Ni/Al₂O₃ after exposure in steam reforming of ethanol (4 kPa C₂H₅OH, and 12 kPa H₂O) for 10 h.

temperature the lattice oxygen (O_x) at the Ce-ZrO₂ surface can oxidize gaseous hydrocarbons (methane (Laosiripojana *et al.*, 2005), ethane (Laosiripojana *et al.*, 2006) and propane (Laosiripojana *et al.*, 2006)). By using Ni/Ce-ZrO₂ as the catalyst, in addition to the reaction on Ni surface, the possible carbon depositions could be inhibited by the gas-solid reactions between these hydrocarbons and the lattice oxygen (O_x) at Ce-ZrO₂ surface forming hydrogen and carbon dioxide, which are thermodynamically unfavored to form carbon species, as illustrated schematically below.



S is the catalyst surface site and CH_x-S is an intermediate surface hydrocarbon species. S can

be considered to be a unique site, or the same site as the lattice oxygen (O_x) (Laosiripojana *et al.*, 2003). During the steam reforming, hydrocarbons are adsorbed on either a unique site (S) or the lattice oxygen (O_x). The lattice oxygen is regenerated by reaction with oxygen containing compounds (steam) present in the system.



4. Influence of operating temperature on the product selectivities

The influence of operating temperature on the product selectivities over Ni/Ce-ZrO₂ and Ni/Al₂O₃ at the inlet C₂H₅OH/H₂O molar ratio of 1.0/3.0 were further studied by varying temperature from 700°C to 1000°C. As shown in Figure 7, it was found that the main products from the ethanol steam reforming over Ni/Ce-ZrO₂ were H₂, CO, CO₂, and CH₄, with small amounts of C₂H₄ and C₂H₆ depending on the operating temperature. In contrast, significant amounts of C₂H₄ and C₂H₆ were also observed as well as other chemical components from the ethanol steam reforming over Ni/Al₂O₃ in the range of conditions studied. Consequently, less H₂, CO, and CO₂ selectivities were achieved over these catalysts. Table 4 presents the quantities of carbon deposited on both catalysts after operated at several temperatures.

For comparison, the conversions and the product selectivities at equilibrium state were

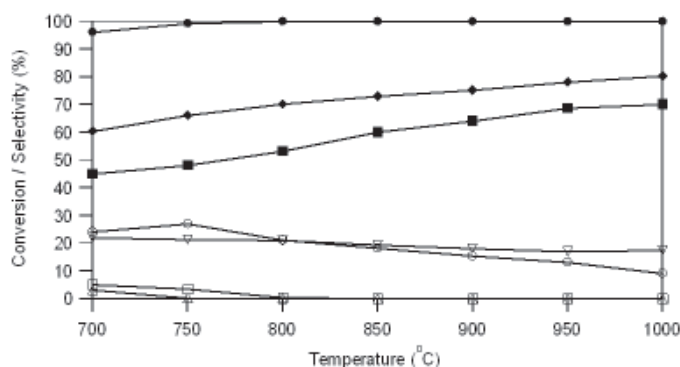


Figure 7(A)

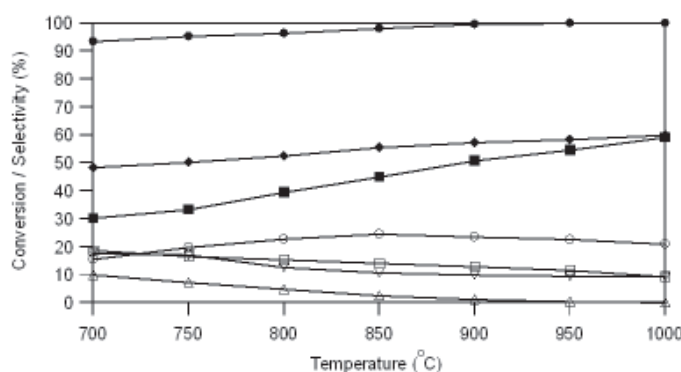


Figure 7(B)

Figure 7. Effect of temperature on the conversion and product selectivities (C₂H₅OH(●), H₂(◆), CO(■), CO₂(∇), CH₄(○), C₂H₄(□), C₂H₆(Δ)) from ethanol steam reforming over Ni/Ce-ZrO₂ (Figure 7a) and Ni/Al₂O₃ (Figure 7b) with inlet C₂H₅OH/H₂O ratios of 1/3.

Table 4. The quantities of carbon deposited on catalysts after operated at several temperatures.

Temperature (°C)	The quantities of carbon deposited (monolayers)	
	Ni/Al ₂ O ₃	Ni/Ce-ZrO ₂
700	5.78a (5.77) ^b	2.08 a (2.04) ^b
750	5.39 (5.31)	1.89 (1.91)
800	5.01 (5.07)	1.66 (1.68)
850	4.74 (4.71)	1.58 (1.55)
900	4.52 (4.54)	1.52 (1.47)
950	4.33 (4.36)	1.37 (1.34)
1000	4.21 (4.20)	1.11 (1.14)

^a Calculated using CO and CO₂ yields from temperature-programmed oxidation (TPO) with 10% oxygen.

^b Calculated from the balance of carbon in the system.

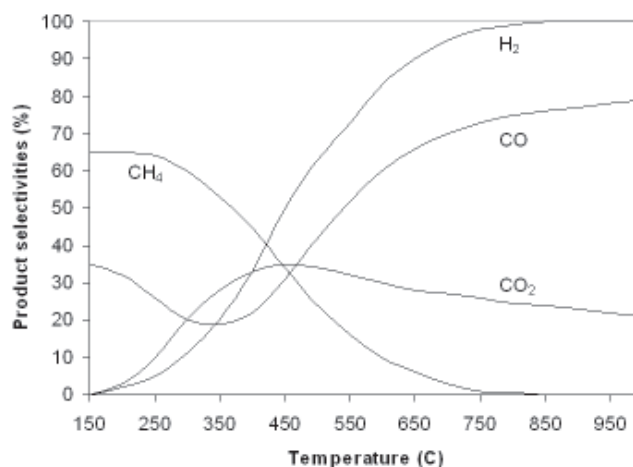


Figure 8. The product selectivities from ethanol steam reforming at the equilibrium level (4 kPa C₂H₅OH, and 12 kPa H₂O).

calculated using AspenPlus10.2 simulation program as shown in Figure 8. Regarding the simulation, the conversions of ethanol at equilibrium level are 100% in the range of temperature between 700-1000°C. The selectivity of hydrogen at equilibrium are slightly higher than those achieved from the experiments over Ni/Ce-ZrO₂, in addition, neither C₂H₆ nor C₂H₄ formation was observed at the equilibrium state in this range of temperature due to the complete reforming of this component to CH₄, CO, and CO₂.

Conclusion

Ni on Ce-ZrO₂ support (Ni/Ce-ZrO₂) provides excellent reactivity toward the steam reforming of ethanol with high resistance toward carbon deposition and better product selectivities compared to Ni/Al₂O₃. The main products from these reforming processes over Ni/Ce-ZrO₂ were H₂, CO, and CO₂ with small amount of CH₄, whereas the formations of C₂H₄ and C₂H₆ were also observed together with the above gas components from the reactions over Ni/Al₂O₃ in the range of conditions studied. These high hydrocarbon compounds are easily formed by the homogenous decomposition of ethanol at high temperature (above 550°C) without the catalyst requirement. The great benefits of Ni/Ce-ZrO₂ in terms of

stability and reactivity toward ethanol reforming, high resistance toward carbon deposition, and good product selectivities are due to the high redox property of Ce-ZrO₂.

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